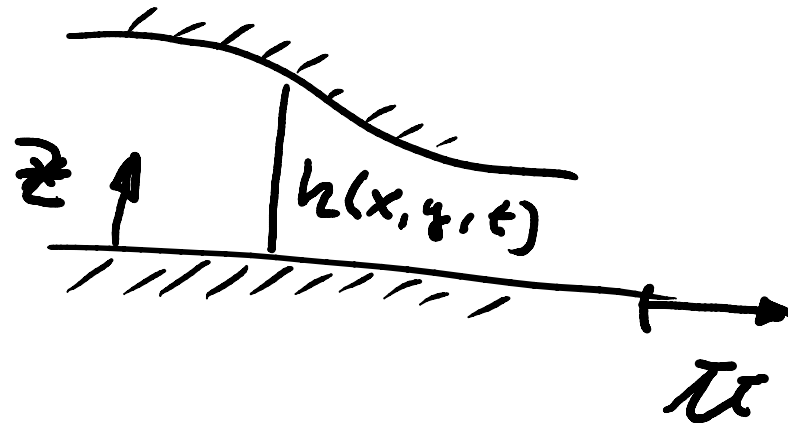


Sommerfeldzahl und Steifigkeit bei Zapfenlagern

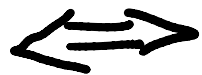
Reynoldische Gleichung der hydrodynamischen Schmierung.

$$\vec{v} = v_x \vec{e}_x + v_y \vec{e}_y$$



Kontin:

$$\nabla \cdot \vec{v} + \frac{\partial h}{\partial t} = 0$$



$$\frac{\partial}{\partial x} \left(\frac{h^3}{2} \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{h^3}{2} \frac{\partial p}{\partial y} \right) = 6 \left[\frac{\partial(\mu h)}{\partial x} + \frac{\partial(\nu h)}{\partial y} + 2 \frac{\partial h}{\partial t} \right]$$

Reynoldische Gleichung = Poisson'sche DGL.
linear 😊



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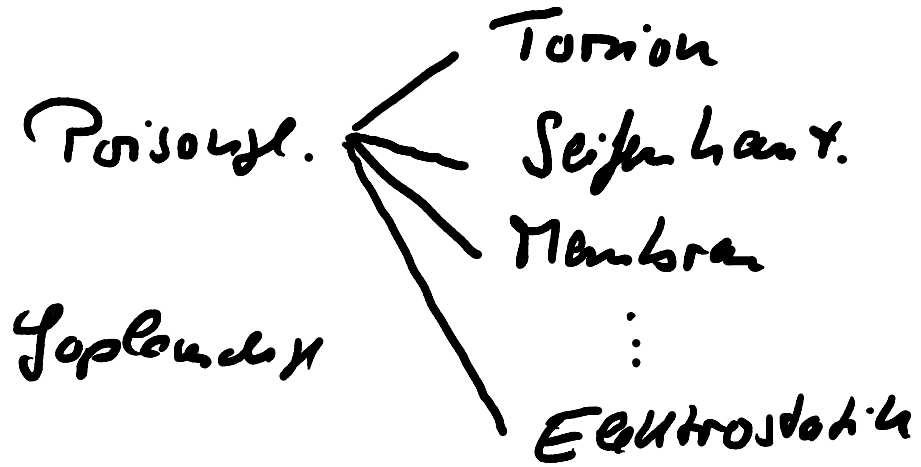


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$$\Delta p = k$$

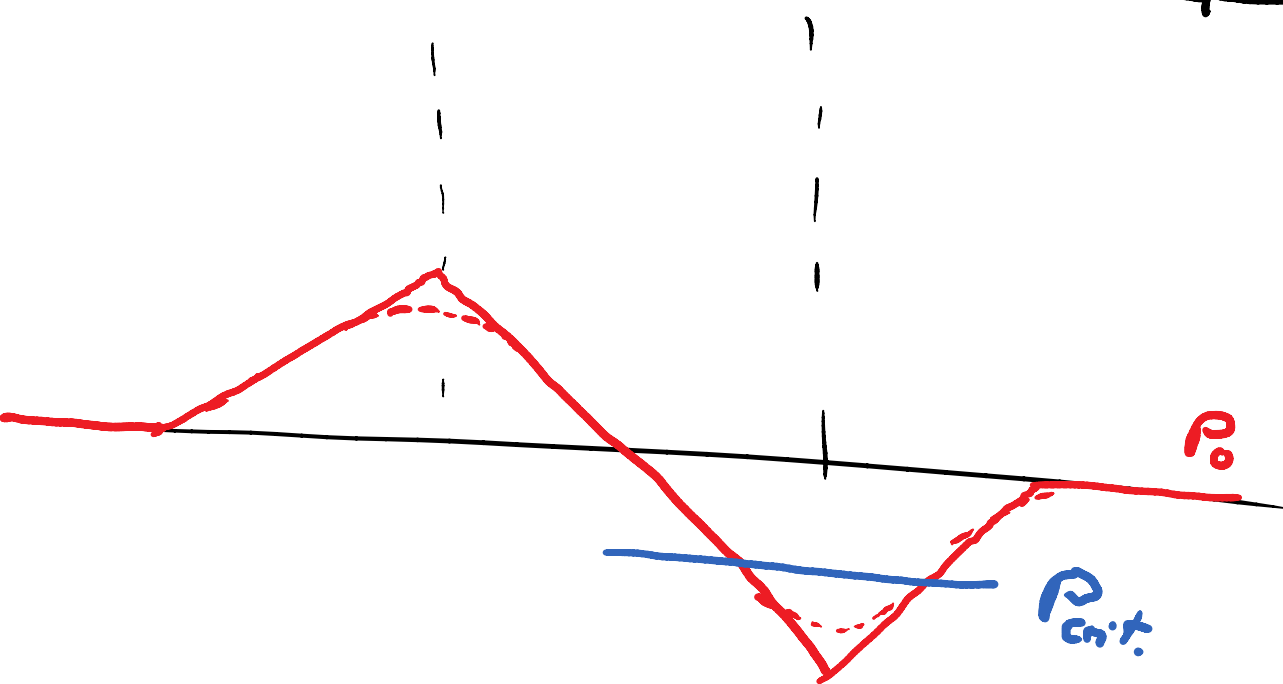
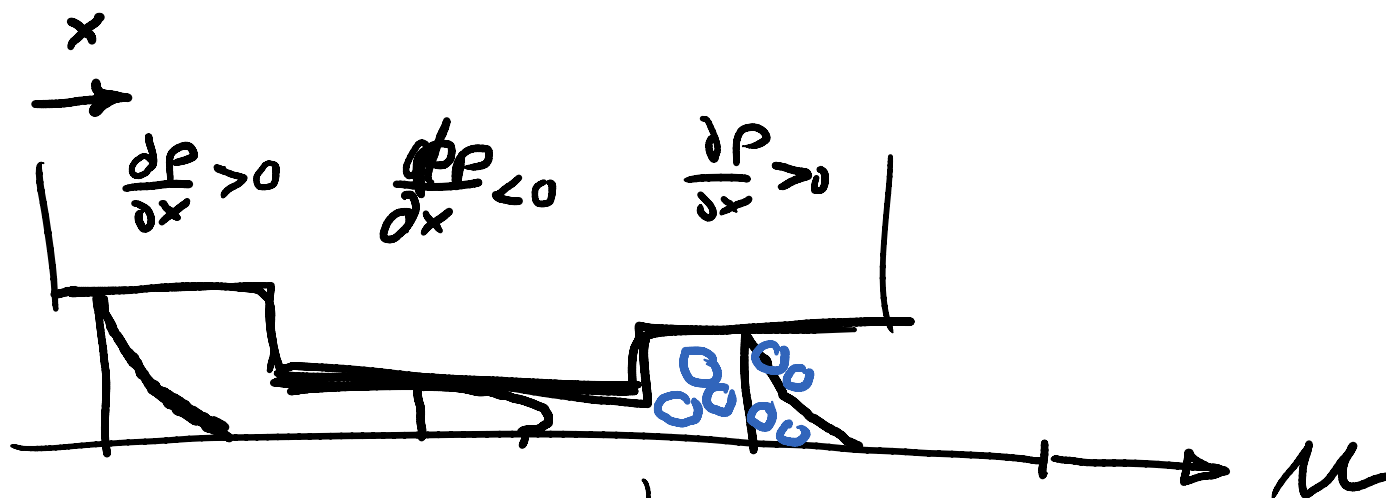
$$\Delta p = \sigma$$



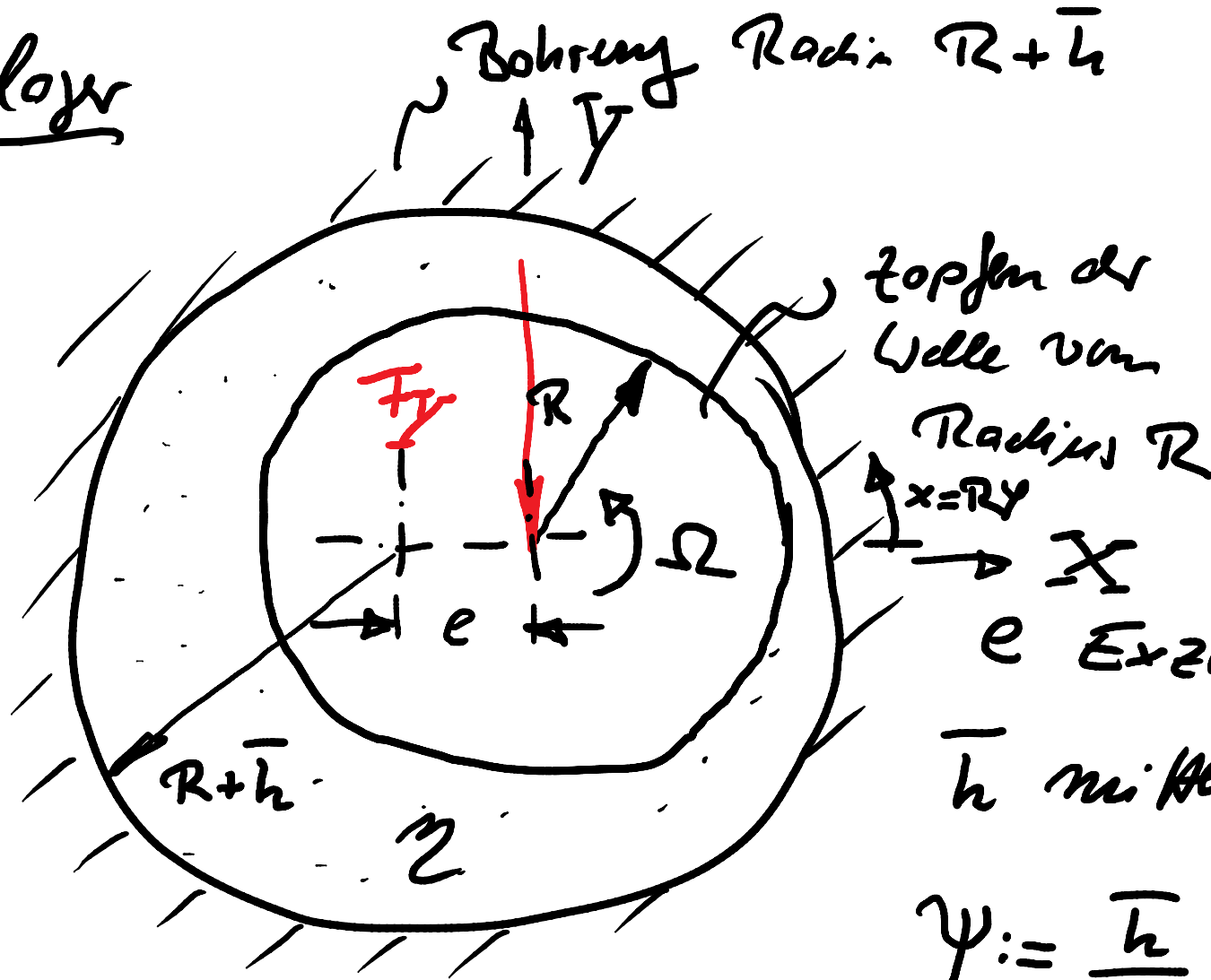
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Zopfenlager



Bohrung Radius $R + \bar{h}$

Zopfen der Welle von Radius R

$x = RY$

e Exzentrizität

\bar{h} mittlerer Spalt

$$\psi := \frac{\bar{h}}{R} \text{ rel. Spalt}$$

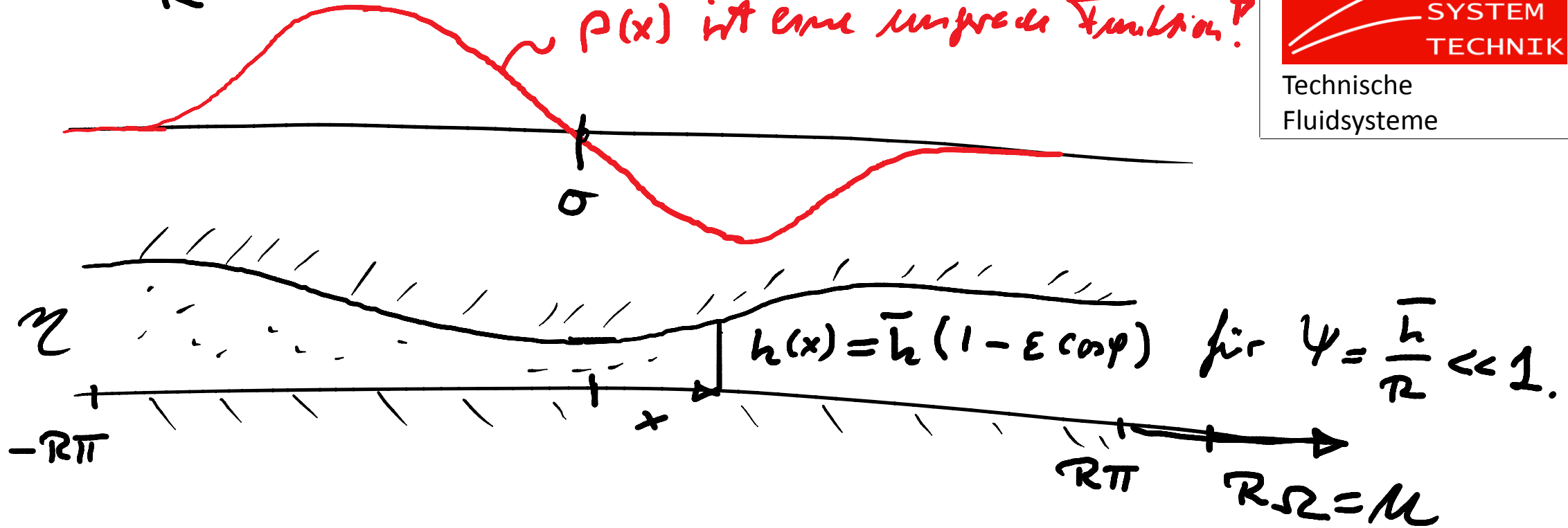
$$\psi \approx 10^{-3}$$





$\varepsilon := \frac{e}{R}$ relative Exzentrizität.

$\rho(x)$ ist eine ungerade Funktion!

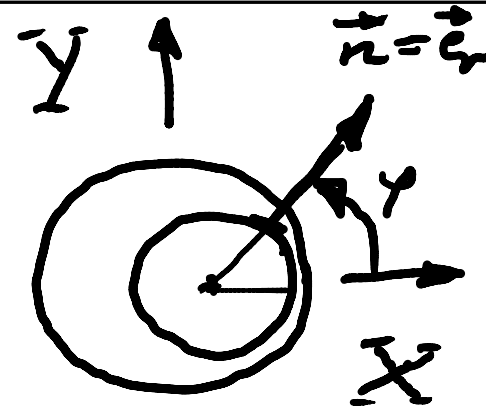


ε ist ein Betriebsparameter.

ψ ist ein konstruktiv vorgegebene Größe.

Kraft pro Tideniveau.

$$\vec{F} = F_x \vec{e}_x + F_y \vec{e}_y$$



$$= \int_0^{2\pi} d\vec{F} = \int_{\mathcal{N}} \underbrace{\vec{t}}_{d\vec{F}} d\mathcal{N} = \int_0^{2\pi} \underbrace{\vec{n} \cdot \vec{T}}_{d\mathcal{N}} R d\varphi$$

$$= \int_0^{2\pi} \vec{e}_r \cdot \left(-\rho \vec{e}_r \vec{e}_r + \underbrace{2\eta \frac{\partial \mu}{\partial r}}_0 \vec{e}_r \vec{e}_r + \eta \frac{\partial \mu}{\partial z} \vec{e}_r \vec{e}_z + \dots \right) R d\varphi$$

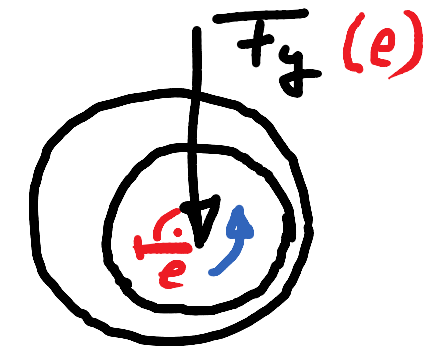
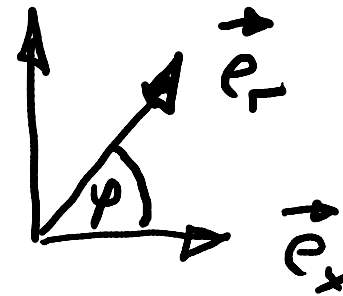
$$= \int_0^{2\pi} \underbrace{-\rho \vec{e}_r}_{\equiv} + \underbrace{\eta \frac{\partial \mu}{\partial z}}_0 \vec{e}_z R d\varphi \quad \left| \begin{array}{l} \cdot \vec{e}_x \rightsquigarrow F_x \\ \cdot \vec{e}_y \rightsquigarrow F_y \end{array} \right.$$



$$\overline{F_x} = \int_0^{2\pi} \underbrace{-p(\varphi)}_{\text{unversch.}} \underbrace{\vec{e}_r \cdot \vec{e}_x}_{\text{versch.}} R d\varphi = 0$$

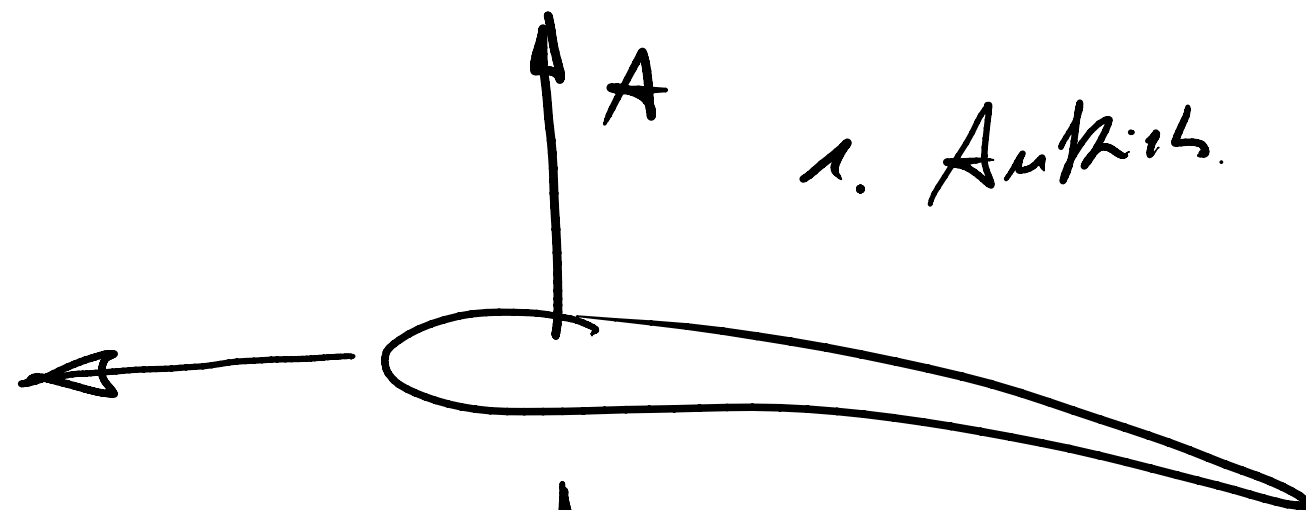
unversch. versch.

versch.

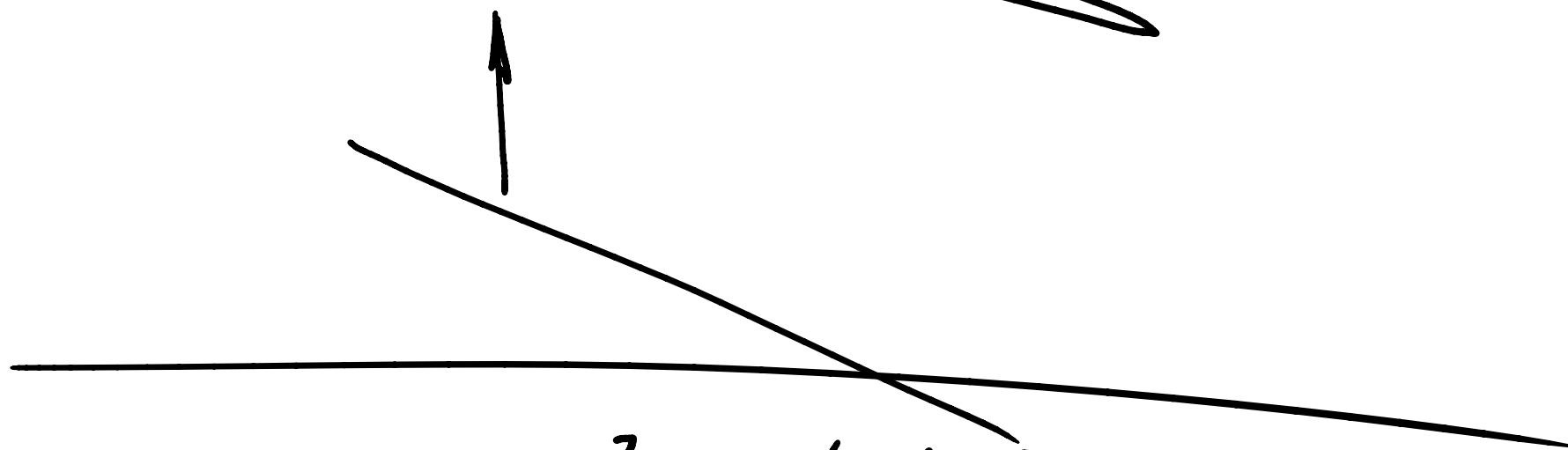


$$\overline{F_y} = \int_0^{2\pi} -p(\varphi) \underbrace{\vec{e}_r \cdot \vec{e}_y}_{\text{versch.}} R d\varphi \neq 0 \rightarrow \text{versch.}$$

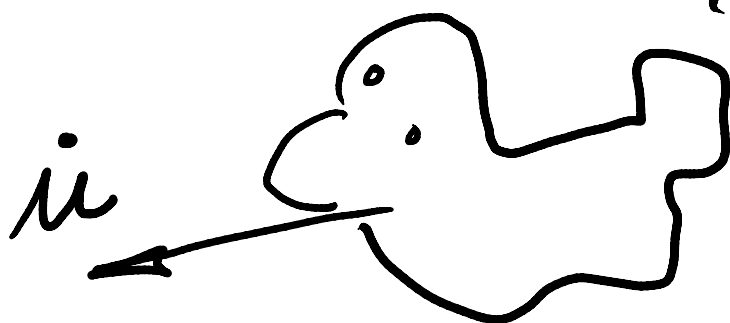
versch.



1. Auftrieb.

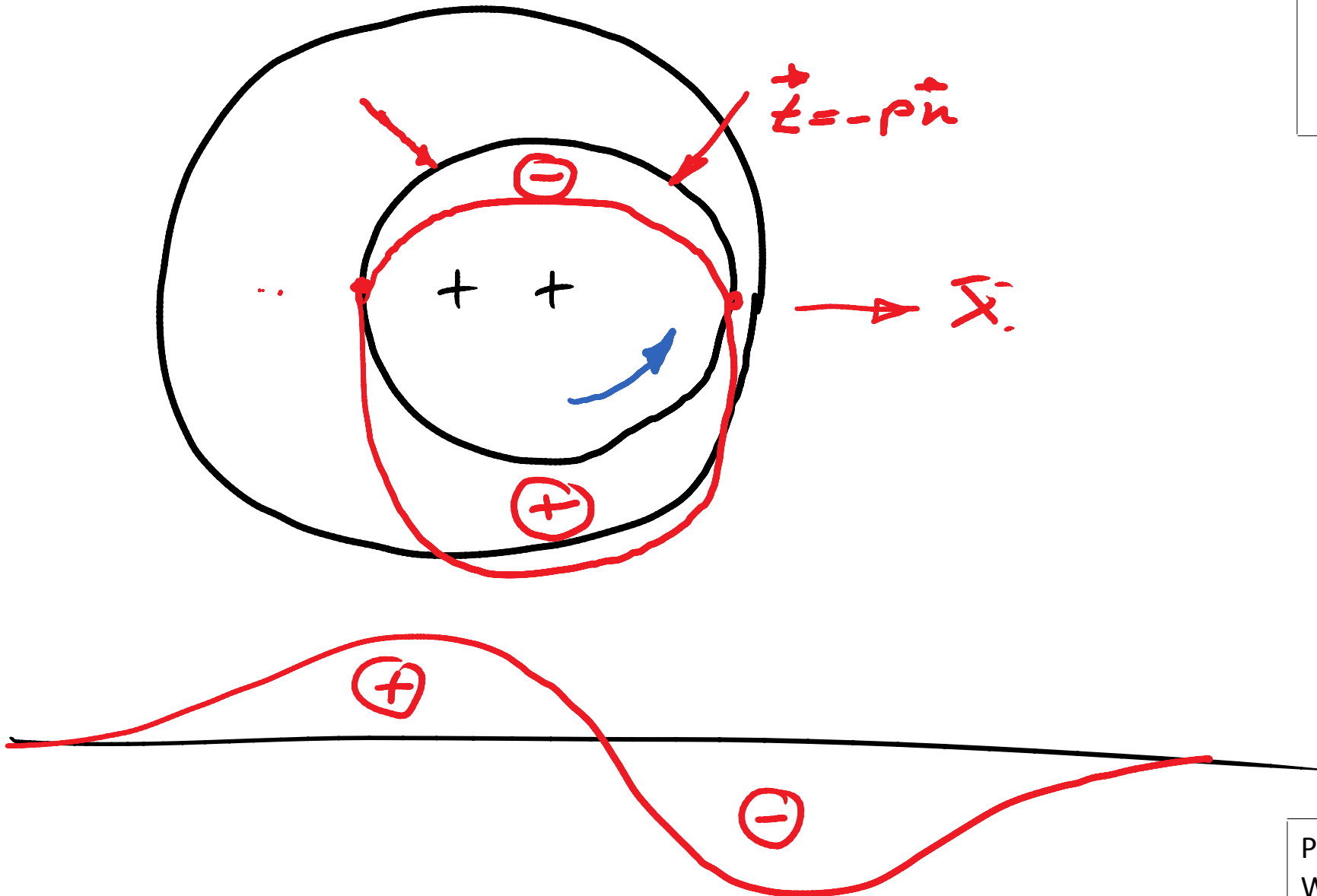


2. Wirbelschleife.



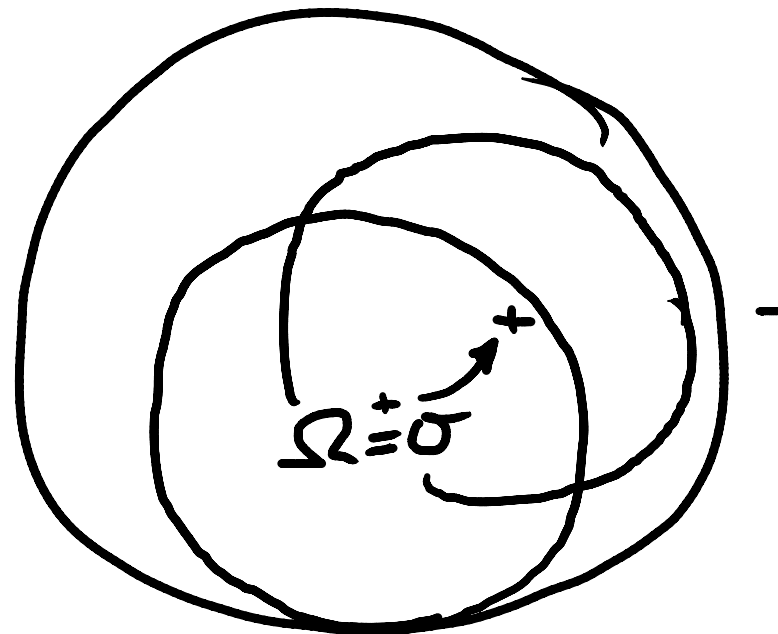
u

3. Leiter



$$\vec{E} = -\rho \vec{n}$$

ξ

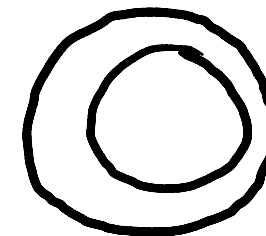




$$F_g = f_h(\Omega, \eta, R, \bar{h}, e, D)$$

	F_g	$\overset{\sim P}{\Omega \eta}$	η	R	\bar{h}	e	D
F	1	1	1				
L		-2	-2	1	1	1	1
T		1	1				

$B \gg R$



D gewöhnl.

Membranl. bzw. Lsg.

$D \ll R$
kurze Lsg.

$$\frac{F_g}{\Omega \eta B R} = f_h\left(\psi, \epsilon, \frac{B}{R}\right)$$



$$\frac{\overline{F_z}}{BR^2 \Omega} = f_4\left(\psi, \varepsilon, \frac{B}{R}\right) \quad 4\text{-Größen}$$

Arnold Summenfeld 1904

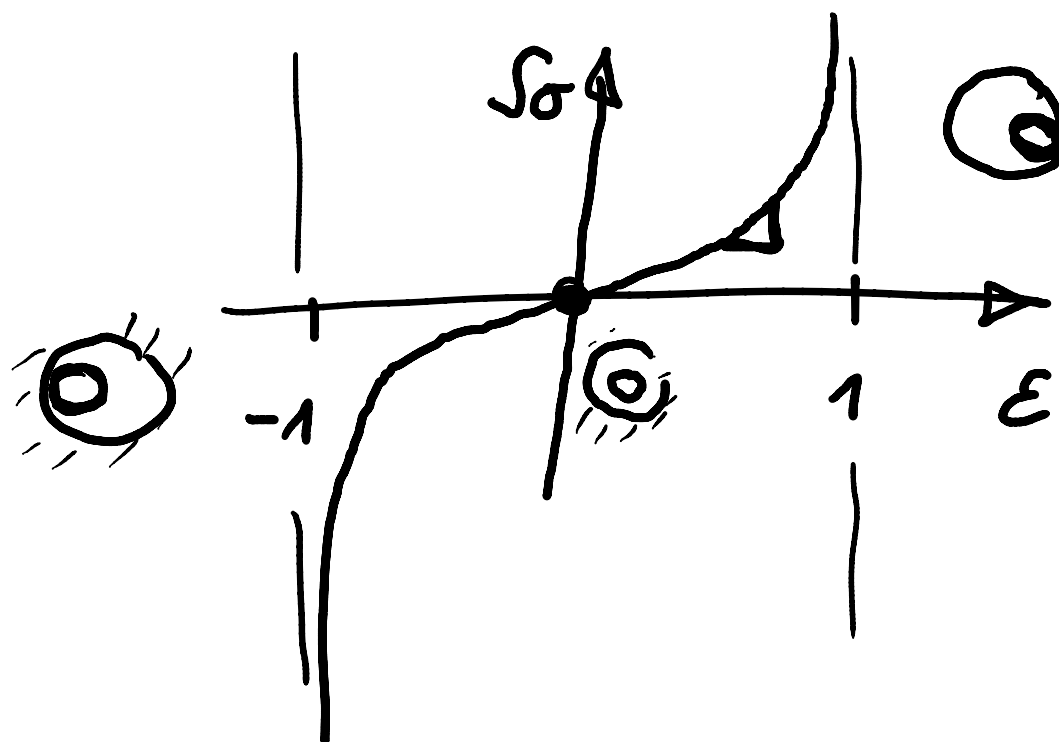
$$\underbrace{\frac{\overline{F_z}}{BR^2 \Omega}}_{\psi^2} = f_4\left(\varepsilon, \frac{B}{R}\right) \quad 3\text{ Größen!}$$

$$\overline{N_o} = f_0\left(\varepsilon, \frac{B}{R}\right)$$



$R/\delta \rightarrow \infty$: $S_\sigma = S_\sigma(\epsilon)$ unendlich
breit

$$S_\sigma = \frac{12\pi\epsilon}{\sqrt{1-\epsilon^2}(2+\epsilon^2)}$$



$$k_+ = \frac{d S_\sigma}{d \epsilon}$$

Geometrischer

$$\epsilon \rightarrow 0 : k_+ \rightarrow 0$$

$\frac{B}{R} \rightarrow \sigma$: kurze Form

~~4g~~
$$S\sigma = \frac{\pi \varepsilon^2}{(1 - \varepsilon^2)^{3/2}}$$

Lit: Spurh, Strängeleu Kap. 5

Spurh, Dimensionen etc.

Sommerfeld Mechanik der deformierbaren Medien.

Vokelpohl.

Pimkus & Sternlicht.



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$$\frac{F_g}{\rho \eta \Omega} = f_4\left(\psi, \varepsilon, \frac{\beta}{\rho}\right)$$

allgemeine Dimensionsanalyse.

Inspektionelle Dimensionsanalyse od. (Spreng)
Methode der Differentialgleich (Zirip)



$$\frac{\partial}{\partial x} \left(\frac{h^3}{2} \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{h^3}{2} \frac{\partial p}{\partial y} \right) = 6 \frac{\partial(\mu h)}{\partial x}$$

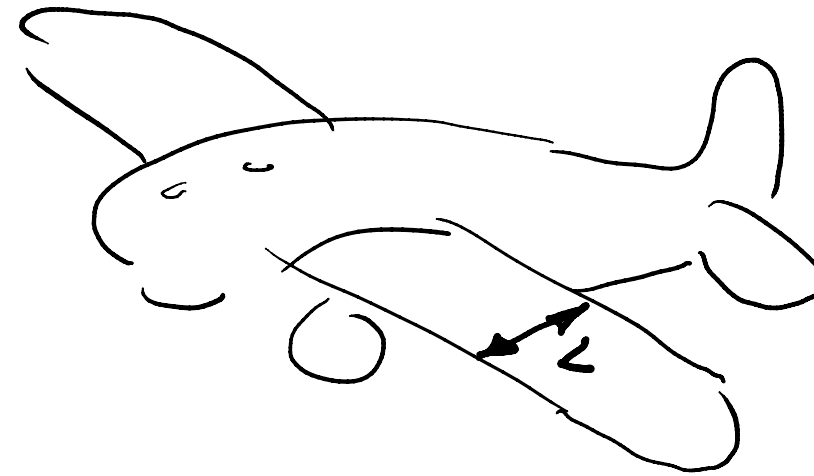
$$y = y + B$$

$$x = x + R$$

$$h = h + \bar{h}$$

$$p = p + \bar{p}$$

$$\mu = \Omega R$$



$$\frac{R}{\Omega R}$$

()₊ dimensionless

$$\frac{6 \Omega R \partial h_+}{R \partial x_+}$$

$$\frac{\bar{h}^3 \bar{p}}{2 R^2}$$

$$\frac{\partial}{\partial x_+} \left(h_+^3 \frac{\partial p_+}{\partial x_+} \right) + \frac{\bar{h}^3 \bar{p}}{2 B^2} \frac{\partial}{\partial y_+} \left(h_+^3 \frac{\partial p_+}{\partial y_+} \right) =$$



$$\left(\frac{h}{R}\right)^2 \frac{\rho}{\rho_0} \underbrace{\frac{\partial}{\partial x_+} \left(h_+^3 \frac{\partial p_+}{\partial x_+} \right)}_{\sigma(1)} +$$

$$\underbrace{\left(\frac{h}{R}\right)^2 \frac{\rho}{\rho_0}}_{\sigma(1)} \underbrace{\left(\frac{R}{B}\right)^2}_{\sigma(1)} \frac{\partial}{\partial y_+} \left(h_+^3 \frac{\partial p_+}{\partial y_+} \right) = \underbrace{6}_{\sigma(1)} \frac{\partial h_+}{\partial x_+}$$

So $\underbrace{\text{Quadrat von } \frac{R}{B}}_{\sigma(1)} = \rho$

Selektieren

$$\frac{\partial}{\partial x} \left(h^3 \frac{\partial p}{\partial x} \right) + \rho^2 \frac{\partial}{\partial y} \left(h^3 \frac{\partial p}{\partial y} \right) = \frac{6}{\rho} \frac{\partial h}{\partial x}$$